

Attenuation / loss in optical fiber is also expressed in terms of decibels per kilometer (dB/km). Fiber attenuation can be described by the general relation:

$$\frac{dP}{dz} = -\alpha P$$

Where α is the power attenuation coefficient per unit length z .

The power light that travels along fibre can be decrease exponentially with distance L :

$$P_{out} = P_{in} e^{-\alpha L}$$

Therefore, the attenuation is conveniently expressed in terms of dB/km as:

$$\alpha (dB/km) = \frac{10}{L} \log_{10} \left(\frac{P_{out}}{P_{in}} \right)$$

Where α is the known as the attenuation coefficient per unit length, (dB/km).

Example: Suppose $-1.75 dB/km$ is the power attenuation coefficient of communication system using $20 km$ of optical fiber. Calculate the loss efficiency in dB ($Loss_{dB}$), and the output power if the input power is $300 mW$.

$$Loss_{dB} = -1.75 \frac{dB}{km} \times 20 km = -35 dB$$

$$Loss_{dB} = 10 \log_{10} \left(\frac{P_{out}}{P_{in}} \right)$$

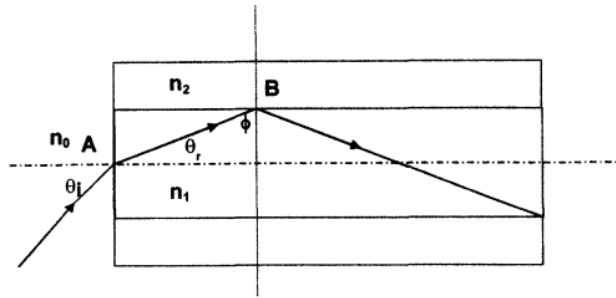
$$-35 dB = 10 \log_{10} \left(\frac{P_{out}}{600 mW} \right)$$

$$P_{out} = 600 mW \times 10^{-\frac{35}{10}}$$

$$\therefore P_{out} = 0.1897 mW$$

Example: Consider a step index fiber with parameters $n_1 = 1.475$, $n_2 = 1.460$, $n_0 = 1$, and core radius $a = 25 \mu m$.

- (a) Calculate the maximum incident angle and numerical aperture (NA) of the fiber.
- (b) Under the maximum incident angle, how many total reflections happen for a 1 km long fiber?
- (b) If the input power is 100 mW and the output power is 90 mW of this 1 km long fiber, what is the total loss for each reflection (in dB)?



(a)
$$NA = \sin \theta_i = \sqrt{n_{co}^2 - n_{cl}^2}$$

$$NA = \sqrt{(1.475)^2 - (1.460)^2} = 0.21$$

(b) From the relationship $n_0 \sin \theta_i = n_1 \sin \theta_r$, internal refractive angle, θ_r , can be calculated as:

$$\theta_r = \sin^{-1} \left(\frac{n_0 \sin \theta_i}{n_1} \right) = \sin^{-1} \left(\frac{1 \times 0.21}{1.475} \right) = 8.19^\circ$$

Then the propagation length for each reflection is $2a / \tan \theta_r$. When L is the length of fiber, the total number of reflections can be calculated as:

$$N = \frac{L}{2a / \tan \theta_r} = \frac{10^3 m}{2.25 \times 10^{-6} m} \times \tan(8.19^\circ) = 2.88 \times 10^6 \text{ times}$$

(c) The total loss (in dB) is:

$$Loss_{dB} = 10 \log_{10} \left(\frac{P_{out}}{P_{in}} \right) = 10 \log_{10} \left(\frac{90 \text{ mW}}{100 \text{ mW}} \right) = -0.458$$

The total loss for each reflection (1 km) = $-0.458 \times 2.88 \times 10^6 = -1.32 \times 10^6$

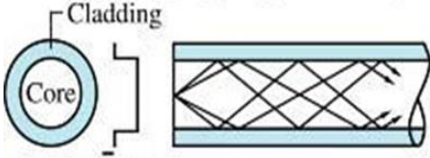
H.W.: Derive the approximation of the Numerical Aperture ($NA \cong n_1 \sqrt{2\Delta}$) for $\Delta \ll 1$. What is the difference in approximate and exact expression for the value of NA if $n_1 = 1.49$ and $n_2 = 1.48$?

Types of Fiber Optic:

In communication systems, there are three basic types of fiber optic:

- Step-index multimode fiber.
- Parabolically-graded-index multimode fiber.
- Step-index single mode fiber.

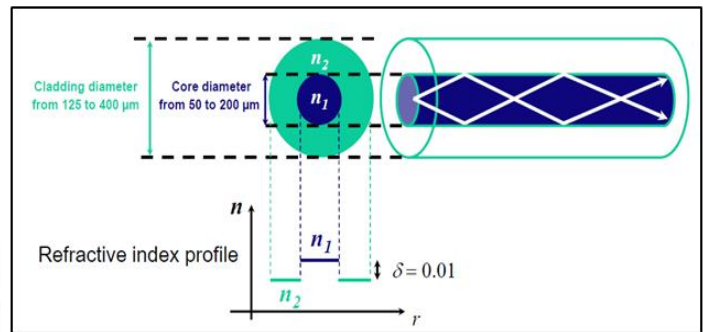
(a) **Step-index multimode fiber**
Simple coupling; large modal dispersion



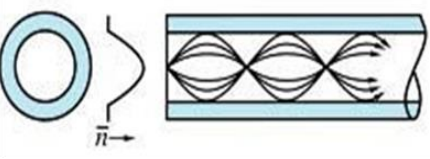
Cladding
Core
 \bar{n}

Typical diameters and refractive indices

Core/cladding diameter	62.5/125, 100/140, ..., 1000/1200 μm
Core index	1.45
Index difference	1% – 2%



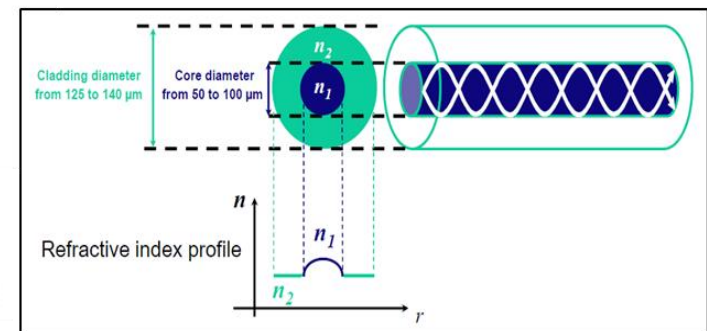
(b) **Parabolically-graded-index multimode fiber**
Simple coupling; difficult fabrication; low or zero modal dispersion



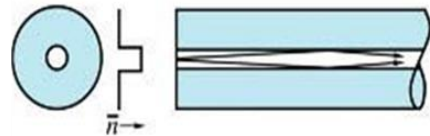
Core/cladding diameter 50/125, 62.5/125, 85/125

Core index at center 1.45

Index difference 1% – 2% in graded index profile



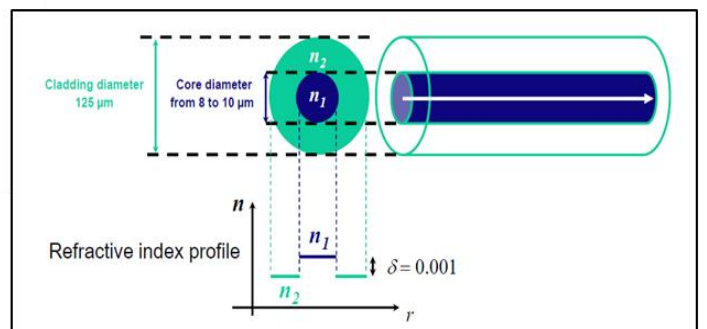
(c) **Step-index single-mode fiber**
Difficult coupling; difficult fabrication; no modal dispersion



Core/cladding diameter 9/125

Core index 1.45

Index difference 1% – 2%



- ❖ Each mode corresponds to a particular ray angle.
- ❖ Hence it is clear that the rays for the different modes will progress at different speeds.
- ❖ This leads to unsatisfactory performance of a telecommunication system.

In general:

▶ Multimode Fiber

- Several signals can be transmitted
- Several frequencies used to modulate the signal

▶ Single Mode Fiber

- only one signal can be transmitted
- use of single frequency

Theory of Light Propagation in Optical Fiber:

- ❖ Geometrical optics can't describe rigorously light propagation in fibers
- ❖ Must be handled by electromagnetic theory (wave propagation)
- ❖ Starting point: Maxwell's equations

$$\begin{aligned} \nabla \times E &= -\frac{\partial B}{\partial T} & (1) \\ \nabla \times H &= J + \frac{\partial D}{\partial T} & (2) \\ \nabla \cdot D &= \rho_f & (3) \\ \nabla \cdot B &= 0 & (4) \end{aligned}$$

with

$$\begin{aligned} B &= \mu_0 H + M & : \text{Magnetic flux density} \\ D &= \epsilon_0 E + P & : \text{Electric flux density} \\ J &= 0 & : \text{Current density} \\ \rho_f &= 0 & : \text{Charge density} \end{aligned}$$

Light Propagation = linear propagation + non-linear propagation.

$$\begin{aligned} P(r,t) &= P_L(r,t) + P_{NL}(r,t) \\ P_L(r,t) &= \epsilon_0 \int_{-\infty}^{+\infty} \chi^{(1)}(t-t_1) E(r,t_1) dt_1 : \text{Linear Polarization} \\ P_{NL}(r,T) &: \text{Nonlinear Polarization} \end{aligned}$$

$\chi^{(1)}$: linear susceptibility

We consider only linear propagation: $P_{NL}(r,T)$ negligible.

$$\nabla \times \nabla \times E(r,t) + \frac{1}{c^2} \frac{\partial^2 E(r,t)}{\partial t^2} = -\mu_0 \frac{\partial^2 P_L(r,t)}{\partial t^2}$$

We now introduce the Fourier transform: $\tilde{E}(r, \omega) = \int_{-\infty}^{+\infty} E(r,t) e^{i\omega t} dt$

$$\frac{\partial^k E(r,t)}{\partial t^k} \Leftrightarrow (i\omega)^k \tilde{E}(r, \omega)$$

And we get: $\nabla \times \nabla \times \tilde{E}(r, \omega) - \frac{\omega^2}{c^2} \tilde{E}(r, \omega) = +\mu_0 \epsilon_0 \chi^{(1)}(\omega) \omega^2 \tilde{E}(r, \omega)$

which can be rewritten as

$$\nabla \times \nabla \times \tilde{E}(r, \omega) - \frac{\omega^2}{c^2} [1 + c^2 \mu_0 \epsilon_0 \chi^{(1)}(\omega)] \tilde{E}(r, \omega) = 0$$

i.e. $\nabla \times \nabla \times \tilde{E}(r, \omega) - \frac{\omega^2}{c^2} \epsilon(\omega) \tilde{E}(r, \omega) = 0$

$$\epsilon(\omega) = \left[n + i \frac{\alpha c}{2\omega} \right]^2 \text{ with } n = 1 + \frac{1}{2} \Re[\chi^{(1)}(\omega)]$$

$$\text{and } \alpha = \frac{\omega}{cn(\omega)} \Im[\chi^{(1)}(\omega)]$$

n : refractive index
 α : absorption

$$\nabla \times \nabla \times \tilde{E}(r, \omega) = \nabla(\nabla \cdot \tilde{E}(r, \omega)) - \nabla^2 \tilde{E}(r, \omega) = -\nabla^2 \tilde{E}(r, \omega)$$

$$(\nabla \cdot \tilde{E}(r, \omega) \propto \nabla \cdot \tilde{D}(r, \omega) = 0)$$

$$\nabla^2 \tilde{E}(r, \omega) + n^2 \frac{\omega^2}{c^2} \tilde{E}(r, \omega) = 0 : \text{Helmoltz Equation!}$$

Each components of $E(x,y,z,t) = U(x,y,z) e^{i\omega t}$ must satisfy the Helmoltz equation

$$\nabla^2 U + n^2 k_0^2 U = 0 \text{ with } \begin{cases} n = n_1 \text{ for } r \leq a \\ n = n_2 \text{ for } r > a \\ k_0 = 2\pi / \lambda \end{cases}$$

Note: $\lambda = \omega / c$