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၎င်းတို့ ပြုစုခဲ့သော အခွင့်အလမ်းများကို အသုံးပြုရန် အဆင်ပြေအောင် အကူအညီ ပေးခဲ့ပါသည်။

samples with distilled water.

The prepared samples of soil were tested after different exposure periods. The test program included determination of shear strength characteristics, consolidation characteristics, and Atterberg limits. The changes in shear strength, coefficient of permeability, void ratio – effective stress relationship, and Atterberg limits were recorded with the change in exposure period or the concentration of pore fluid solution. Generally, it was found that there are reductions in the shear strength of soil when its pore fluid is changed from distilled water to solutions of used salts or raw sewage. Also it was found that there is a change in the calculated values of permeability, upon changing the type of pore fluid. The coefficient of consolidation for polluted soil was found to be less than that for the reference of salts were used with different concentration (0.25, 0.5, 0.75, 1.0 normality).

The effect of pore fluid chemistry on the engineering properties of soil in Garmatt-Ali zone of Basrah was investigated. The tested soil is described as silty clay of low plasticity. The pore fluid was altered to include distilled water, raw sewage, and solutions of various salts such as calcium carbonate, magnesium sulphate, and calcium chloride. Also, the solutions

Abstract

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TIOS

PROPERTIES OF BASRAH (GARMATT ALI ZONE) CLAY

EFFECT OF POLLUTION ON THE MECHANICAL

products may be in gas, liquid or solid form. The most important gases are carbon dioxide (CO₂), carbon monoxide (CO), nitrogen dioxide (NO₂) and sulfur dioxide (SO₂).⁽⁴⁾ Another type of pollutants that have effects on the engineering properties of soil is salts.

Mathewson⁽⁵⁾ found that calcium carbonate act as a source of calcium which leads to reducing osmosis stress (osmotic potential) between the water of soil and the clay layers. Also, he pointed out that the existence of calcium carbonate leads to lowering the value of plasticity index through its action as a carnivore materials to the deposit granules or they form covers for the granules. AL-Rawi et al.⁽⁶⁾ reported that the depression of some soils is attributed to its high content of calcium carbonate. Daham⁽⁷⁾ pointed out that the existence of calcium carbonate increases the deposit shearing resistance by forming covers surrounding deposit granules, so it stops the activity of salts and increases the attractive force between the particles of deposit. Giroud and Bottero⁽⁸⁾ illustrated that the existence of chloride ion in deposits causes increase of its compressibility because of chloride salts

Experimental Work

In this study, the tested soil was taken from Garmatt-Ali zone of Basrah.

existence such as sodium chloride causes flocculation processes and increasing in liquid limit. AL-Yasry⁽⁹⁾ studied the effect of calcium chloride on soil permeability and found that the soil permeability increases with increasing calcium chloride content. The shear strength of soil, on one hand, is one of the most important characteristics of many soil mechanics problems such as stability of slopes, ultimate bearing capacity, lateral earth pressure, and friction developed by piles. On the other hand, the consolidation of a soil stratum and subsequent settlement of the superstructure, also play an important role in foundation engineering. The objective of this study is to examine the effect of changing the pore fluid chemistry on the shear strength, consolidation characteristics, and Atterberg limits of Basrah (Garmatt Ali zone) soil. The used pore fluids include raw sewage and solutions of different salts such as calcium carbonate, magnesium sulphate, and calcium chloride. Samples of soil are mixed with these fluids at the saturation level and then tested after different exposure periods.

Generally, Basrah soils consist of soft and compressible stratum. Samples were collected, manually, from the upper 1.5m of soil strata. The disturbed samples of soil

were packed in three bags (50-60)kg each and transported to the soil mechanics laboratory at university of Basrah. The excavating process was performed using a mechanical excavator (shovel). The specific gravity for soil specimens was determined according to ASTM D854-58.⁽¹⁰⁾ The liquid and plastic limits tests were performed according to ASTM D424-59 and ASTM D43-66⁽¹⁰⁾ respectively. Grain size distribution was determined according to ASTM D422-79.⁽¹⁰⁾ A set of sieves ranging in size from NO.4 to NO.200 was used and a pan was placed under the set to collect all grains passing NO.200 sieve. Hydrometer analysis (a sedimentation test) was used for soils passing sieve NO.200, The grain size distribution was determined according to ASTM D422-79⁽¹⁰⁾. The grain size distribution curve of soil sample is shown in Figure (1). According to the unified soil classification system, the soil is classified as (CL), silty clays of low plasticity. Unit weight and water content test were performed according to ASTM D2216-80 and ASTM D2927-71.⁽¹⁰⁾ The moisture content was determined as the percentage of the mass of free water that can be removed from a material, usually by heating at 105°C⁽¹¹⁾. The moisture content-dry density relationship of soil was obtained by the standard Proctor compaction tests following the procedure

of ASTM 1557-79.⁽¹⁰⁾ The unconsolidated undrained triaxial compression test(UU) was carried out according to ASTM D 2166-85⁽¹⁰⁾ using a constant strain compression machine with a rate of speed 1mm/min. Consolidation and swelling test were carried out according to (ASTM D2435-70)⁽¹⁰⁾ by using odometer cell. The period of test was 6 days for 6 load increments, each load was left for 24 hours. After the last increment was left on 24 hours, unloading was started by lowering the load every one hour. and swelling index reading were recorded. The results of these tests for the natural soil are shown in Table (1). Table (2) illustrates the composition of the studied soil. The results were obtained by x-ray diffraction analysis. The test was carried out by the state company of the geological survey and mining in Basrah.⁽¹²⁾ The chemical analysis of the soil was also carried out by the state company of the geological survey and mining in Basrah and the results are depicted in Table(3). The characteristics of raw sewage were determined at the same day of collecting it and are summarized in Table(4). Hydrogen ion activity (pH) was measured using PW 94.18- PHILIPS meter.⁽¹³⁾ Electrical conductivity (EC) was measured using TOA-CM-8ET-JAPAN meter.⁽¹³⁾ Total suspended solids (TSS) and total dissolved solids (TDS) were measured according to

standard method (13). Biological oxygen demand (BOD₅) was measured using the

Preparation of Samples

The natural disturbed soil obtained from the site had been oven dried and manually pulverized. The specified amount of fluids, to reach the saturation level, was added at room temperature in low stream and sewage, and solutions of various salts such as calcium carbonate, magnesium sulphate, and calcium chloride.

Four different types of fluids had been used as a soil pore fluid in this study. These fluids are:

- 1) Distilled water
- 2) Calcium carbonate (CaCO_3) solution
- 3) Magnesium sulphate (MgSO_4) solution
- 4) Calcium chloride (CaCl_2) solution
- 5) Raw sewage

The concentrations of salt solutions were 0.2N, 0.5N, 0.75N, and 1.0N for the shear strength test and 0.5N and 1.0N for the consolidation test and Atterberg limits testes.

The specimens were tested after different time intervals from remolding. Table(5) gives the details of salts concentrations and period of exposure used in this study along with the results of UU and consolidation test

method (Winkler Azide Modification).⁽¹³⁾

thoroughly mixed by hand with the dry soil until uniform paste was obtained. The paste, then, was remolded into a sufficient number of large samples which were waxed and stored until the time of test. The fluids used included distilled water, raw

Results and Discussion

Atterberg Limits and Indices

The index properties of the natural soil used in this study are shown in Table (6). The liquid limit is (44), the plastic limit is (34) and the plasticity index is (10) for the natural soil, therefore this soil can be classified according to the (unified classification system) as silty clay of low plasticity (CL). The concentration of calcium carbonate in this natural soil is (0.21)Normality, calcium chloride is (0.09)Normality and magnesium sulphate is (0.25)Normality.

After the soil is mixed with the used salts in different concentrations the index properties become as depicted in Table (6). This table and Fig. (2) illustrate the effect of calcium carbonate on index properties of soil. It can be noticed that when adding this salt the value of liquid limit and plasticity index is larger than that of the natural soil. This may be because of the calcium carbonate as a powder dose not

conductivity which are associated to low porosity and to deficient internal drainage.

(14)

Shear Strength of Soil

The results of unconsolidated undrained (UU) triaxial compression tests for soils polluted by salts are shown in Tables

(7),(8), and (9).

Figure (5) illustrates the variation of

shear strength (C_u) of soil with time for

two samples, in the first the pore fluid is

distilled water while in the second is raw

sewage.

The shear strength (C_u) of soil with

distilled water is 24.45 kN/m^2 and the

internal angle of friction is $\phi_u=0$. (C_u) is

found to increase with time The shear

resistance of a soil in an undisturbed

condition may be considerably greater than

its strength after being remoulded at the

same moisture content. The shear strength

of the remoulded sample frequently

increases with time after remoulding

without any change in moisture content. (15)

The entire undisturbed strength may not be

regained. This strength regain has been

explained either by changes in particle

arrangement and antiparticle forces, or by

changes in adsorbed water.

Adding raw sewage to the investigated

soil leads to increase of shear strength of

soil as compared to the reference sample

dissolve in water which leads to increase the surface area of clay soil then to increase the water content that is needed to reach the saturation state. However

increasing the salt concentration from 0.5N to 1.0N causes the L.L and P.L. to decrease.

Also it is clear that the plastic limit of salted soil is lower than that of the natural soil, due to that any type of added

materials to the natural soil will adsorb some water from the natural soil. The effect of adding calcium chloride to the

natural soil on the atterberg limits is shown in Table (6) and Fig. (3). The same behavior is noticed for soil polluted for soil

polluted with this salt as that of calcium carbonate. Table (6) and Fig. (4) illustrate the

effect of magnesium sulphate on atterberg limits of the tested soil. It can be noticed that the liquid limit and plasticity index for

polluted soil are larger than those of the natural soil, and the plastic limit is lower than that of the natural soil. Also it can be

noticed that the liquid limit and plasticity index increase with the increase of magnesium sulphate concentration, while

plastic limit remains constant with increasing that salt concentration. This result can be justified since the magnesium

ion restricts the movement and availability of water. Soils with high (Mg) are soils having high water retention, slow to very slow infiltration rate and hydraulic

(Fig. 5). This increase may be attributed to that the organic chemicals.⁽¹⁶⁾ which exist in raw sewage, dissociate in water to produce cations which may have complex structure. These large organic cations are adsorbed to clay surfaces in cation exchange reactions, replacing smaller inorganic cations, that are present. From Tables (7),(8), and (9) it can be seen that the values of C_u of the soil polluted by the three salts $CaCO_3$, $MgSO_4$, and $CaCl_2$ are less than that for reference sample. Also C_u decreases as the exposure time increases. Increasing the concentration of $MgSO_4$ and $CaCl_2$ solutions from 0.25N to 1.0N leads to a decrease of C_u values, while increasing the concentration of $CaCO_3$ solution causes an increase of C_u of soil.

The reduction in shear strength of polluted soils may be attributed for each salt as follows:

1- to the more developed flocculated structure, where some ions (Ca or CO) may replace the ions which are originally present on the clay surface. The resultant flocculated structure is expected to have high void ratio⁽¹⁷⁾.

2- to that the magnesium is highly hydrated and the magnesium ions have high water retention then causing clay peptization and affecting the porosity and the hydraulic conductivity of the soil⁽¹⁸⁾.

3- to the high soluble of calcium chloride in water that leads to dispersion of the soil and then increases the permeability and consequently decreases the shear strength of soil⁽²⁾.

Consolidation properties of soil

Table (10) gives the consolidation characteristics of the soil with different pore fluids. It can be seen that the consolidation coefficient (C_v) and compression index (C_c) decrease for the polluted soil as compared with the reference sample having the distilled water as pore fluid. These results are due to the precipitation of different salts in voids between the particles of soil. However, increasing the concentration of the three used salts from 0.5N to 1.0N leads to increase C_v and C_c although their values remain below those for the reference sample.

The effect of pore fluid chemistry on the swelling index (C_s) is also illustrated in Table (10). C_s increases for soils polluted with $MgSO_4$ solution as compared with the reference sample. Increasing the concentration of this solution from 0.5N to 1.0N leads to further increase in C_s . However, 0.5N solutions of $CaCO_3$ and $CaCl_2$ in addition to the raw sewage causes C_s to decrease. Increasing the concentration of solutions of these two

salts to 1.0N increases C_s to larger value than that for reference sample.

Figures (6) and (7) shows the relationships between the effective stress and void ratio for soils treated with distilled water, raw sewage and CaCO_3 solutions. As compared with the reference soil sample with distilled water, the void ratio is larger for soil polluted by raw sewage and smaller for soil polluted by CaCO_3 solutions. Increasing the concentration of CaCO_3 solution from 0.5N to 1.0N further decreasing the void ratio of soil. This may be attributed to the precipitation of calcium carbonate in the soil voids.

Conclusions

Based on the present experimental investigation, and limited to both the materials tested and the tests procedures employed, the following conclusions could be drawn:

- 1- The shear strength of soil is affected upon by both type and concentration of the chemicals in the pore fluid and the time of exposure to these chemicals.
- 2- Generally, there are reductions in the shear strength of soil when its pore fluid changed from distilled water to CaCO_3 solution, MgSO_4 solution, and CaCl_2 solution .

- 3- The shear strength of soil with pore fluid of CaCO_3 , MgSO_4 , and CaCl_2 solutions decreases as the time of exposure increases.
- 4- When the pore fluid is the raw sewage the shear strength of soil increases with the time of exposure, but it remains smaller than the natural soil.
- 5- The increase of concentration of solution of leads to an increase of shear strength of soil in case of CaCO_3 and a reduction in shear strength for both MgSO_4 and CaCl_2 .
- 6- The consolidation coefficient (C_v) and the compression index (C_c) decrease when the pore fluid changes from distilled water to solutions of CaCO_3 , MgSO_4 , CaCl_2 , and raw sewage. For high concentration of salts (C_v) and (C_c) values tends to increase considerably.
- 7- For the case of MgSO_4 solution the swelling index (C_s) of soil increases higher than the value of soil mixed with distilled water. However, for other solutions C_s value is lesser than that of reference sample.
- 8- One – dimensional consolidation of the samples of different pore fluids showed that the relationship

between voids ratio and logarithm of consolidation stress is dependent on both the type and concentration of the chemicals in the pore fluid.

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Property	Value
Depth of sampling(m)	1.5
Liquid limit L.L.(%)	44
Plastic limit P.L.(%)	34
Plasticity Index P.I.(%)	10
Specific Gravity (GS)	2.65
Passing NO.200 sieve(%)	51
Unified Classification system	CL
Natural moisture content (%)	21
Bulk density (gm/cm ³)	2.0
Dry density (gm/cm ³)	1.66
Saturation density (gm/cm ³)	2.05
Optimum moisture content (%)	19.73
Maximum dry density (gm/cm ³)	1.635
Saturation moisture content %	32
Voids ratio(original)	0.6

Table (1) Engineering properties of investigated soil

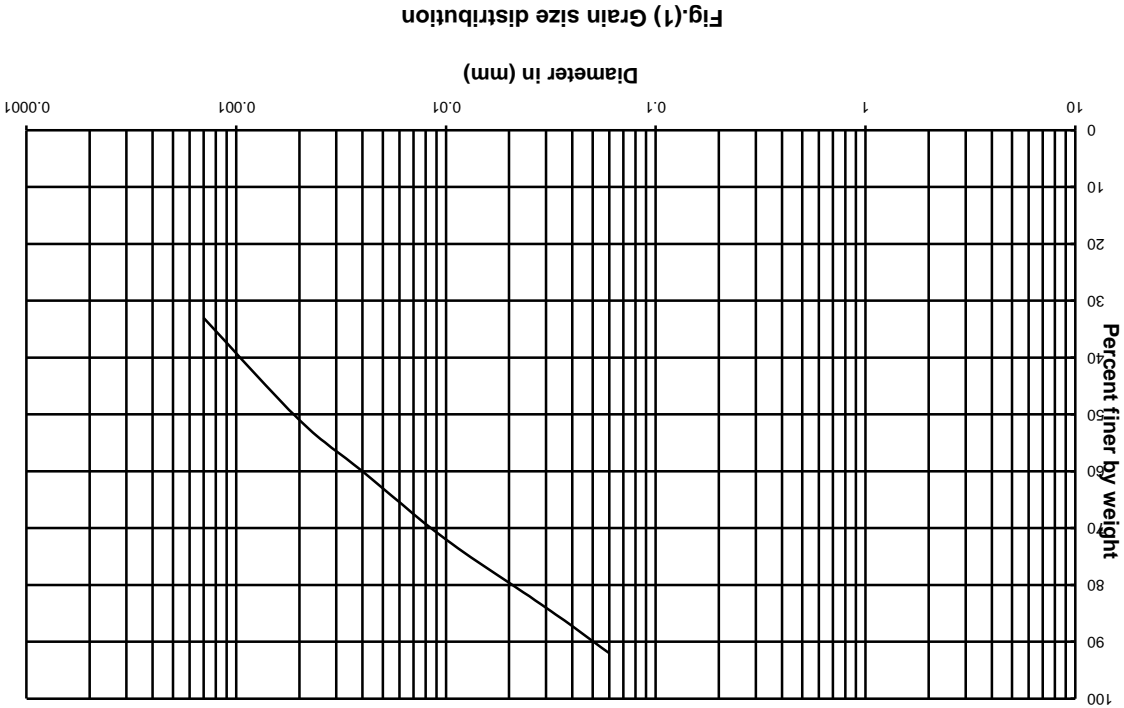


Table (2) Mineral analysis of investigated soil

Mineral	Rate %	Clay Mineral	other Minerals
Montmorillonite	12		
Kaolinite	2		
Illite	8		
Playorskite	7		
Chlorite	2		
Calcite	18.8		
Gypsum	1.1		
Quartz	37		
halite	1.1		
feldspar	4		

Table (3) Chemical Analysis of Investigated Soil

Parameter	Value
Mg (%)	0.1300
Ca (%)	1.7222
CL (%)	0.24282
HCO ₃ (%)	0.0183
CO ₃ (%)	0
pH	7.81
Cu (%)	7*10 ⁻⁴
Mn (%)	0.034796
Z (%)	0.0023
Na (%)	0.5370
K (%)	0.0896
Total salts %	1.856
Organic matter %	0.284
Ni (%)	0.064699
Pb (%)	11*10 ⁻⁴
Cd (%)	18*10 ⁻⁴
CaCO ₃ (Normality)	0.21
MgSO ₄ (Normality)	0.25
CaCl ₂ (Normality)	0.09

Table (4) Raw Sewage Characteristics

Parameter	Value	Permissible
pH	8.00	6.5-9.2
T.S.S.	1000 mg/l	500
T.D.S.	600 mg/l	1500
BOD ₅	50 mg/l	>12
EC	1040 mg/sec	2600

Table (5) Material Concentration and Period of Exposure

Material	Concentration	Test		Period of exposure					
Distilled water		UU	X	X	X	X	X	X	X
		Consolidation	X	-	-	-	-	-	-
Raw sewage		UU	X	X	X	X	X	X	X
		Consolidation	X	-	-	-	-	-	-
CaCO ₃	0.25N	UU	X	X	X	X	X	X	X
		Consolidation	-	-	-	-	-	-	-
	0.5N	UU	X	X	X	X	X	X	X
		Consolidation	X	-	-	-	-	-	-
	0.75N	UU	X	X	X	X	X	X	X
		Consolidation	-	-	-	-	-	-	-
	1.0N	UU	X	X	X	X	X	X	X
		Consolidation	-	-	-	-	-	-	-
MgSO ₄	0.25N	UU	X	X	X	X	X	X	X
		Consolidation	-	-	-	-	-	-	-
	0.5N	UU	X	X	X	X	X	X	X
		Consolidation	X	-	-	-	-	-	-
	0.75N	UU	X	X	X	X	X	X	X
		Consolidation	-	-	-	-	-	-	-
	1.0N	UU	X	X	X	X	X	X	X
		Consolidation	-	-	-	-	-	-	-
CaCl ₂	0.25N	UU	X	X	X	X	X	X	X
		Consolidation	-	-	-	-	-	-	-
	0.5N	UU	X	X	X	X	X	X	X
		Consolidation	X	-	-	-	-	-	-
	0.75N	UU	X	X	X	X	X	X	X
		Consolidation	-	-	-	-	-	-	-
	1.0N	UU	X	X	X	X	X	X	X
		Consolidation	-	-	-	-	-	-	-

h : hour

w : week

x : test is done

- : test is not done

Table (6) Atterberg Limits for Natural and Polluted Soil Samples for 24 Hours Period of Exposure

Type of Soil	Concentration normal	Liquid Limit	Plastic Limit	Plasticity Index
Soil with distilled water	Natural	44	34	10
Soil polluted by CaCO_3	0.5N	55	29	26
	1.0N	46	30	16
Soil polluted by CaCl_2	0.5N	46	21	25
	1.0N	43	24	19
Soil polluted by MgSO_4	0.5N	51	27	24
	1.0N	58	27	31

Fig. (2) Effect of Calcium Carbonate on Atterberg Limits

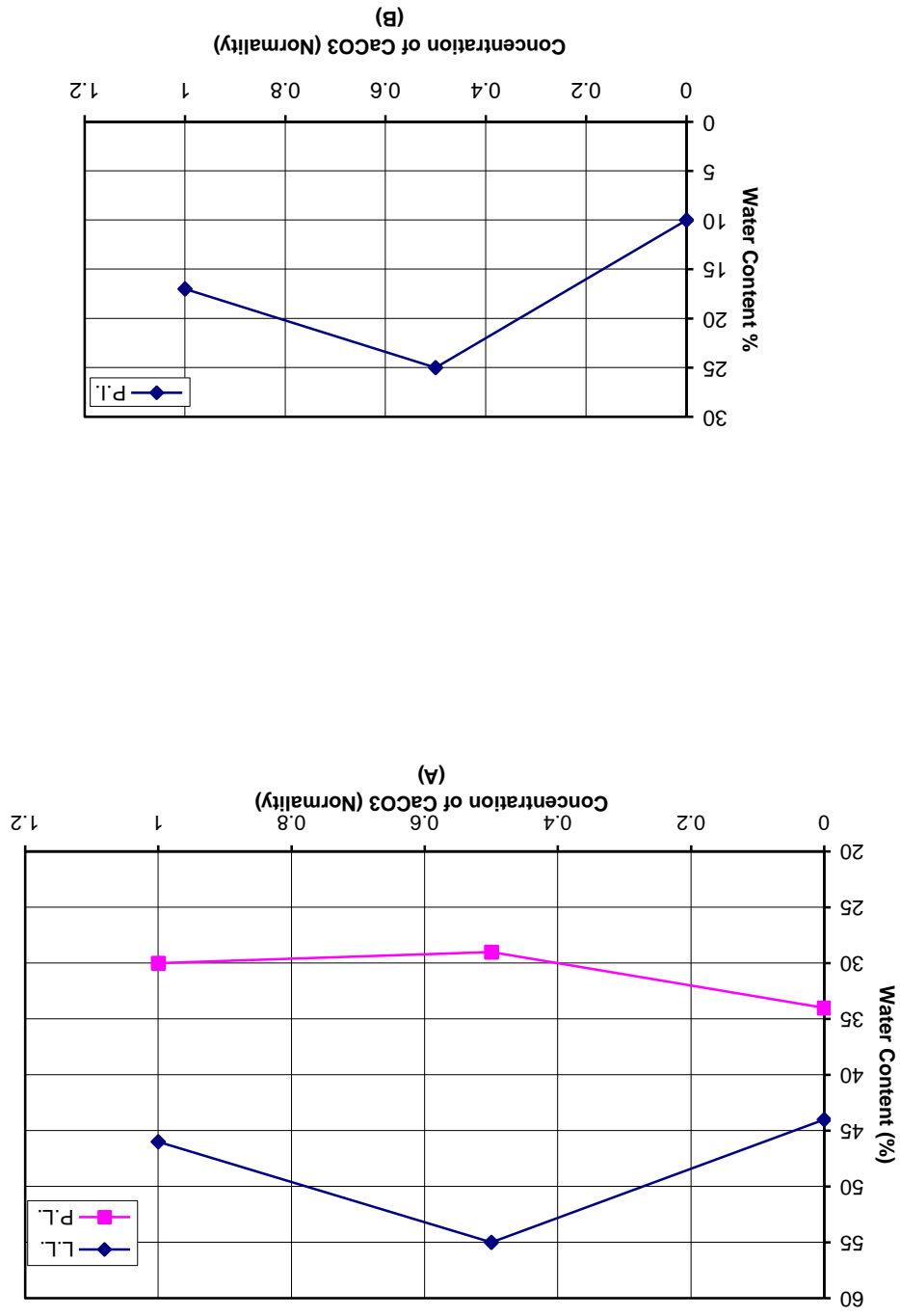


Fig (3) Effect of Calcium Chloride on Atterberg Limits

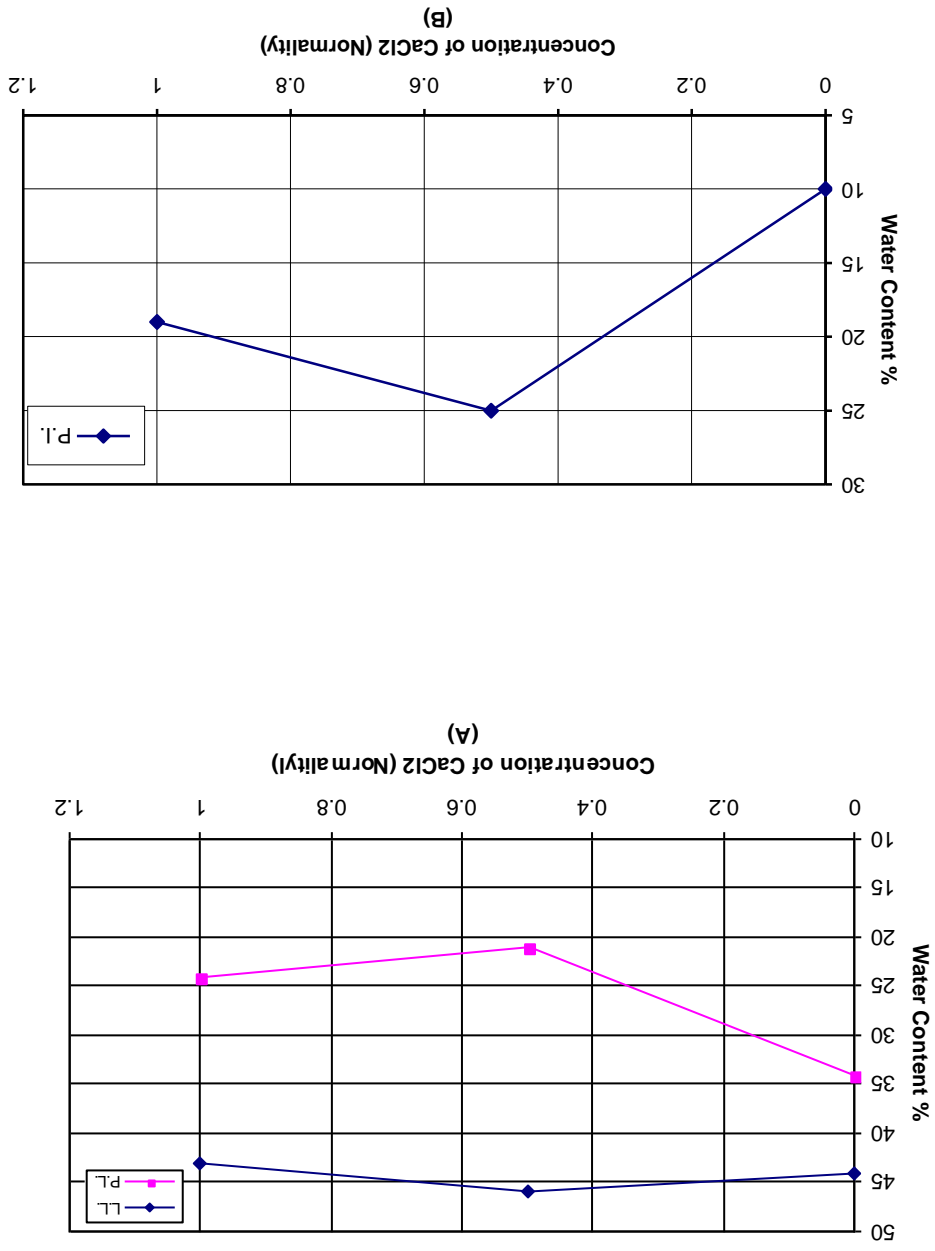


Fig (4) Effect of Magnesium Sulphat on Atterbarg Limits

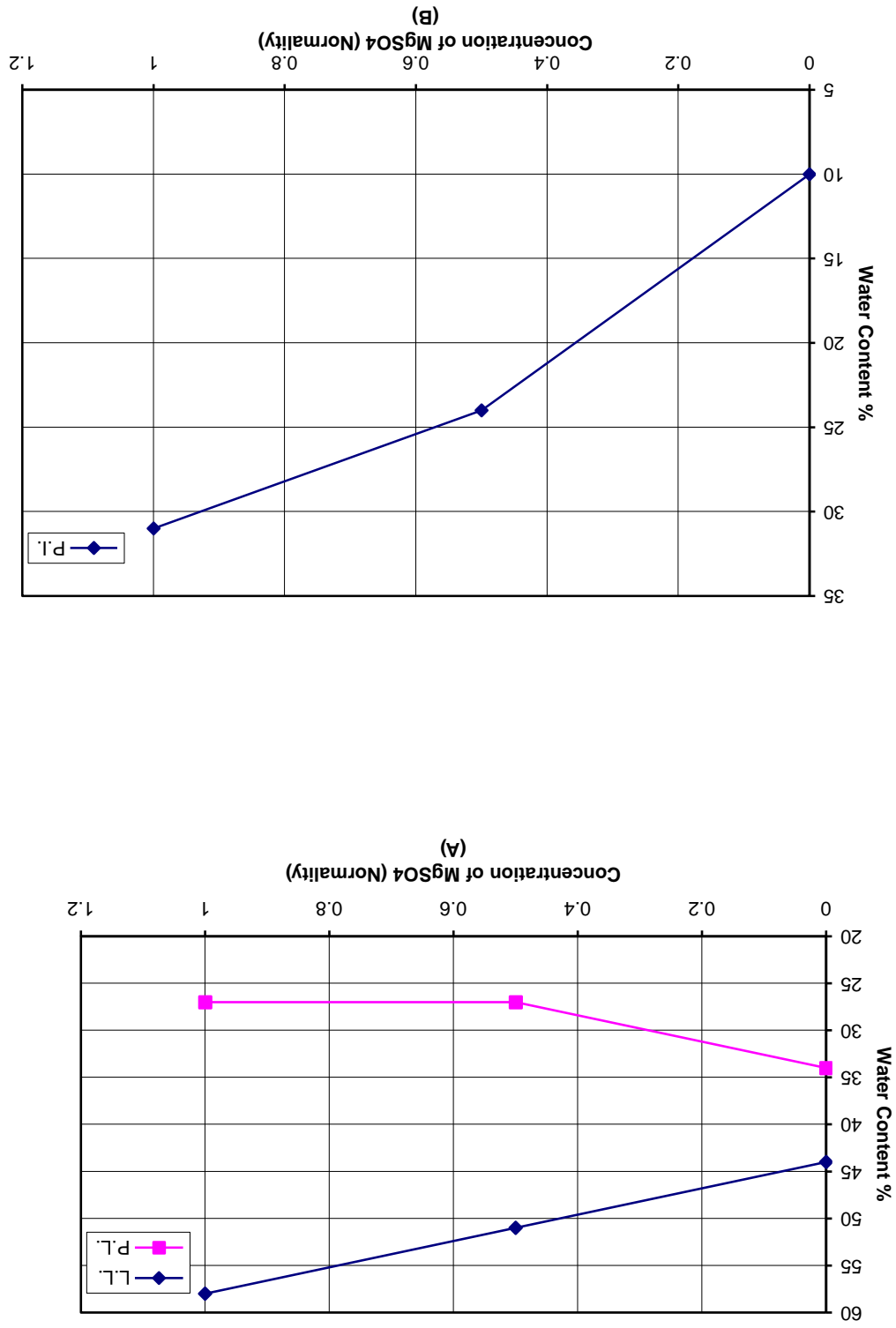


Table (7) Shear strength of soil polluted by calcium carbonate

Concentration of Salts	Value of (Cu) kN/m ²											
	24 Hours		1 week		2 weeks		3 weeks		4 weeks		5 weeks	
	Individual	Average	Individual	Average	Individual	Average	Individual	Average	Individual	Average	Individual	Average
0.25 N	19.8	20.2	12.2	12.5	11.7	12.1	11.85	11.95	11.6	11.8	11.2	11.5
	20.1		12.4		12.0		11.9		11.8		11.6	
	20.7		12.9		12.6		12.1		12.0		11.7	
0.5 N	20.53	20.4	13.4	13.75	13.0	13.27	12.9	13.07	12.7	13.0	12.85	12.95
	20.4		13.85		13.3		13.0		12.9		12.9	
	20.6		14.0		13.51		13.3		13.4		12.8	
0.75 N	20.2	20.5	13.5	14.0	13.4	13.65	13.1	13.35	13.0	13.3	12.8	13.13
	20.6		13.9		13.8		13.3		13.25		13.1	
	20.7		14.6		13.75		13.65		13.65		13.49	
1.0 N	20.3	20.6	14.2	14.6	13.4	14.0	13.5	13.75	13.3	13.5	13.25	13.45
	20.7		14.6		14.1		13.8		13.4		13.35	
	20.8		15.0		14.5		13.95		13.8		13.75	

Table (8) Shear Strength of Soil Polluted by Magnesium Sulphate

Concentration of Salts	Value of (Cu) kN/m ²											
	24 Hours		1 week		2 weeks		3 weeks		4 weeks		5 weeks	
	Individual	Average	Individual	Average	Individual	Average	Individual	Average	Individual	Average	Individual	Average
0.25 N	20.0	24.3	18.9	19.55	17.5	18.0	12.5	13.1	11.8	12.3	11.0	11.5
	24.0		19.6		18.2		12.8		12.2		11.6	
	29.5		20.2		18.3		13.9		12.9		11.9	
0.5 N	20.2	20.7	18.2	18.6	16.9	17.5	11.8	12.15	10.7	11.2	9.9	10.2
	20.6		18.4		17.6		12.0		11.1		10.3	
	21.3		18.6		17.9		12.65		11.8		10.4	
0.75 N	17.5	18.0	17.2	17.5	16.3	16.5	10.7	11.0	9.8	10.3	6.9	7.4
	17.9		17.5		16.5		10.9		10.4		7.5	
	18.6		17.8		16.7		11.4		10.7		7.7	
1.0 N	16.1	16.5	15.9	16.3	15.4	15.8	9.8	10.3	8.8	9.4	5.9	6.6
	16.6		16.4		15.7		10.2		9.2		6.4	
	17.0		16.6		16.3		10.9		10.1		7.5	

Table (4.4) Shear Strength of Soil Polluted by Calcium Chloride

Concentration of Salts	Value of (Cu) KN/m ²											
	24 Hours		1 week		2 week		3 week		4 week		5 week	
	Individual	Range	Individual	Range	Individual	Range	Individual	Range	Individual	Range	Individual	Range
0.25 N	16.9	17.4	14.0	14.5	12.8	13.25	10.5	10.75	9.3	9.8	8.2	8.7
	17.5		14.6		12.1		10.8		9.7		8.5	
	17.9		14.9		13.85		10.95		10.4		9.4	
0.5 N	15.2	15.7	13.5	14.0	12.4	12.65	9.7	9.95	9.0	9.25	7.4	7.7
	15.6		13.8		12.7		9.9		9.3		7.7	
	16.3		14.7		12.85		10.25		9.45		8.0	
0.75 N	14.1	14.4	12.7	13.0	10.96	11.35	9.2	9.4	8.3	8.6	6.7	7.0
	14.3		12.9		11.25		9.4		8.5		6.9	
	14.8		13.4		11.83		9.6		9.0		7.4	
1.0 N	11.32	11.52	9.53	9.89	7.4	7.85	6.25	6.95	6.15	6.55	5.5	5.8
	11.41		9.8		7.9		6.75		6.5		5.8	
	11.83		10.35		8.25		7.85		7.0		6.2	

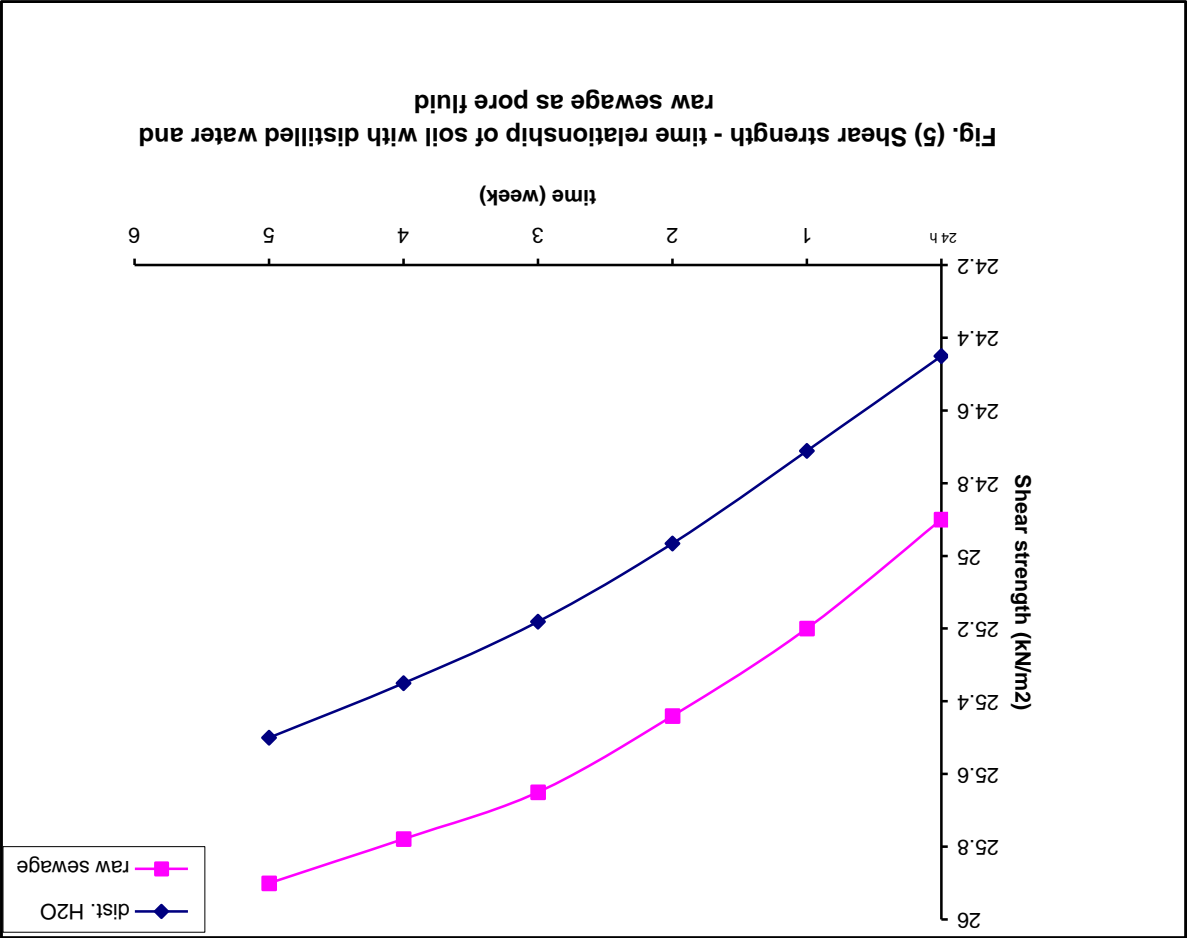


Table (10) Consolidation Characteristics of Clay Soil

1.0 N	CaCl ₂	4.350	0.230	0.060
	MgSO ₄	4.792	0.252	0.075
	CaCO ₃	2.526	0.283	0.048
0.5 N	CaCl ₂	1.380	0.190	0.030
	MgSO ₄	1.586	0.203	0.056
	CaCO ₃	0.883	0.274	0.010
concentration	Raw sewage	1.783	0.22	0.029
	Distilled water	6.113	0.296	0.043
	Fluid types	C _v m ² /year	C _c	C _s

